



Article Classical Thermodynamic Analysis of D-Based Nuclear Fusion Reactions: The Role of Entropy

Silvano Tosti D

ENEA, Fusion and Technology for Nuclear Safety and Security Department, Via E. Fermi 45, 00044 Frascati, Italy; silvano.tosti@enea.it

Abstract: In this work, the feasibility of nuclear processes is studied via classical thermodynamics by assessing the change in entropy, a parameter that has so far been neglected in the analysis of these reactions. The contribution of the entropy to the reaction spontaneity plays a different role in the fission and fusion reactions. In particular, in fusion reactions the temperature acts as a very powerful amplifier of the entropic term $(-T \Delta S)$ that, at the temperature of tokamaks (millions Kelvin), may significantly reduce the thermodynamic spontaneity of these processes. A new approach is followed for assessing the feasibility of the D-based reactions of interest for the magnetically confined nuclear fusion through the investigation of the effect of the temperature on both kinetics and thermodynamics. The results confirm that the deuterium-tritium reaction is the most promising fusion reaction to be realized in tokamak devices. At the temperature of 1.5×10^8 K (\approx 13 keV), the DT reaction exhibits a large thermodynamic spontaneity ($\Delta G = -16.0 \text{ MeV}$) and its reactivity is of the order of $10^{-22} \text{ m}^3/\text{s}$, a value capable of guaranteeing the tritium burning rate needed to operate the nuclear plants under tritium self-sufficiency conditions and with a net energy production. The other results show that at the tokamaks' temperature the two branches of the DD reaction exhibit a modest spontaneity (ΔG around -2 MeV) coupled to very low reactivity values (10^{-24} m³/s). The temperature rise that could be aimed to increase the reactivity is however ineffective to improve the reaction feasibility since it would augment the entropic term as well, thus shifting the ΔG towards positive values. The D³He reaction is soundly spontaneous at the tokamaks' temperature (ΔG values of -17.2 MeV) while its kinetics is close to that of the DD reactions, which are at least two orders of magnitude lower than that of the DT reaction.

Keywords: entropy of nuclear reactions; classical and statistical thermodynamics; deuterium-based fusion reactions

1. Introduction

Strategic foresight analyses deem global warming to be a key future megatrend capable of threatening the sustainable development of humankind [1]. In 2021, fossil fuels, which are mainly responsible for CO_2 and the other greenhouse gases (GHG) released into the atmosphere, represent 82% of the world's energy consumption, with coal, the most polluting source, having a share of about 27% [2]. The reduction of CO_2 and GHG emissions as well as the further penetration of renewable energy sources and other innovative technologies are considered urgent to be actions to strengthen the global response to the climate change trend [3].

Accordingly, worldwide energy strategies are aimed to advance the penetration of renewable sources (solar, photovoltaic, biomass) and the use of cleaner energy vectors (namely hydrogen) [4–8]. Because of their intermittent and discontinuous availability, renewable sources need efficient energy storage systems and their share of 100% is unrealistic. In this view, nuclear power, which presently is the second-largest source of low-carbon electricity, could effectively contribute to the achievement of sustainable energy goals [9]. Furthermore, nuclear power provides diversity in electricity and in primary energy supply



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Copyright: © 2023 by the author. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). and contributes to making electricity systems more flexible and enhancing energy security. Nevertheless, new investments and lifetime extensions of nuclear power plants are often hindered by poor public acceptability, which has been strongly affected firstly by the occurrence of severe accidents and secondly by a nuclear fuel cycle producing a large amount of radioactive and toxic waste [10,11].

The present nuclear power plants exploit fission reactions in which heavy nuclei split into smaller fragments and the difference of mass between reactants and products (i.e., the "defect of mass") corresponds to the energy made available by the process. Diversely from fission, in nuclear fusion light nuclei are combined to form heavier atoms and, also in this case, an amount of energy corresponding to the "defect of mass" is released. As an important aspect, nuclear fusion is potentially cleaner than fission as it does not produce long-living radioactive waste and its fuel cycle uses abundant materials (namely deuterium and lithium). In this perspective, fusion may produce electricity in an inherently safe and inexhaustible way, complying with the requirements for the environmental sustainability of the future energy policies [12–14].

Despite the encouraging expectations for the development of renewable and sustainable energy systems, the realization of fusion power plants has to face very tricky hurdles both in physics and technology [15–19]. The fuel of the most studied fusion reactors consists of a plasma of hydrogen isotopes and helium operated at low pressure and temperature over 10^8 K. This hot plasma, confined by magnetic fields, is subjected to extremely large temperature gradients (about 10^8 K/m) that raise important issues on the integration of physics and technology [19]. The practical feasibility of nuclear fusion must tackle important technological challenges that concern the development of materials capable of withstanding high temperatures and heat fluxes and to resist neutron-induced damage. From a physical standpoint, the main challengers concern the control of the complex behavior of the magnetized plasma and its instability induced by the above-mentioned temperature gradients [19].

The comparison of the historical development of fission and fusion could help to appraise their different levels of feasibility. From the final evidence of the uranium fission in December 1938 in Berlin, the development of fission power plants occurred in less than 20 years: the first commercial pressurized water reactors, the APS-1 reactor in USSR and the Shippingport reactor in U.S.A., started operation in June 1954 and December 1957, respectively. Since the demonstration of uncontrolled thermonuclear fusion corresponding to the first H-bomb explosion in November 1952, a significant amount of fusion power has been produced worldwide in a controlled manner in numerous experiments without, however, achieving a remarkable net energy gain [19]. The International Thermonuclear Experimental Reactor (ITER) is the most important ongoing project aimed to confirm the feasibility of exploiting magnetic confinement fusion for the production of energy through an integrated demonstration of the physics and technology required for a fusion power plant [20].

In this work, the feasibility of a nuclear process is studied through the classical thermodynamics: in particular, this work considers the different role in fission and fusion reactions of the entropy, a parameter that has so far been neglected in the analysis of nuclear reactions. Until now, the analysis of nuclear reactions has been based on the assessment of its exothermicity (the amount of energy released) and reaction rate [21]. The amount of energy released is expressed by the Q_{value} that corresponds, through the Einstein's equation, to the mass defect that, in turn, is calculated as the difference between the total mass of reactants and that of the products of the reaction. The reaction rate, i.e., the number of reactions per unit time and per unit volume, is a parameter related to the probability of the reaction and, therefore, to its kinetics.

By applying the classical thermodynamics, it results that the entropic contribution to the reaction spontaneity plays a different role in the fission and fusion reactions [22,23]. The operation of the plasmas at a very high temperature, adopted to increase the reaction rates in magnetically confined fusion machines, may significantly reduce the thermodynamic

spontaneity of these processes. Consequently, this work introduces a new model for assessing the feasibility of the deuterium-based (D-based) reactions of interest for the magnetically confined nuclear fusion through the investigation of the temperature effect on both the kinetics and thermodynamics.

2. Theory

According to Einstein's equation, an amount of energy corresponding to the masses' difference of reactants and products ("defect of mass") is released during a nuclear reaction:

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$$=\Delta m c^2, \tag{1}$$

where Δm is the "mass defect" and c is the speed of the light.

This energy term, called Q_{value} , is a parameter that can effectively determine the feasibility of a nuclear process. In fact, when the Q_{value} is positive the reaction is exothermic and the process is considered to take place spontaneously.

Considering that most of the energy released from a nuclear reaction is in the end changed into heat, the Q_{value} may correspond to the change in enthalpy (ΔH) unless the sign, as discussed in the following sections. In fact, due to the different rules adopted in nuclear physics and classical thermodynamics, a positive Q_{value} (meaning that energy is released from the process) corresponds to a negative ΔH :

$$Q_{\text{value}} = -\Delta H \tag{2}$$

The exothermicity is a condition used to check between the occurrence of fission or fusion reactions. The distribution of the average binding energy (B) per nucleon (neutron or proton) vs. the mass number (A) is shown in Figure 1. Such a curve exhibits a maximum at A = 56 by distinguishing two regions. In fact, nuclear reactions are exothermic ($Q_{value} > 0$) when the final products have a B/A larger than that of the reagents and, accordingly, two kinds of reactions can be identified in the graph of Figure 1. Below A = 56, light atoms merge to form a heavier nucleus and, therefore, fusion reactions take place while, over A = 56, heavy nuclei split into smaller fragments and fission reactions occur.



Figure 1. The distribution of the average binding energy per nucleon (neutron or proton) vs. the mass number (see also Ref. [22]).

It is noteworthy to discuss how this general feasibility criterion, which relies on the energy released from the process, is correlated to the thermodynamic analysis of nuclear reactions.

2.1. Classical Thermodynamics Analysis of Chemical Processes

The classical thermodynamics is a theory commonly adopted in the analysis of chemical processes. The preliminary design of the process units of chemical plants is carried out through simplified procedures based on thermodynamic calculations. For example, classical thermodynamics studies examine the spontaneity of a process through the evaluation of the Gibbs free energy (G, J mol⁻¹), which is defined by:

$$G = H - T S$$
(3)

where H is the enthalpy (J mol⁻¹), T (K) the temperature, and S the entropy (J mol⁻¹ K⁻¹). For a given reaction, at a constant temperature and pressure the change in G can be calculated by:

$$\Delta G = \Delta H - T \Delta S \tag{4}$$

The change in Gibbs free energy is given by the energy released by the system (Δ H) minus the entropic term (T Δ S). Specifically, a reaction occurs spontaneously when Δ G is negative, meaning that the amount of energy made available to produce work ($-\Delta$ G) corresponds to the energy released ($-\Delta$ H = Q_{value}) net of the entropic contribution (T Δ S).

The assessment of these thermodynamic functions (G, H, S) is usually the first approach for designing the chemical plant units [24]. In fact, the energy balances of the process units are determined by the assessment of the change in enthalpy while the mass balances are derived from the concentrations of the reactants and products calculated through the relationship:

$$\Delta G = -RT \ln K_{eq} \tag{5}$$

where R is the gas constant (8.31 J mol⁻¹ K⁻¹) and K_{eq} (dimensionless) is the equilibrium constant given by the ratio at the chemical equilibrium of the activities (or molar concentrations) of the product species over those of the reactant species involved in the chemical reaction, taking stoichiometric coefficients of the reaction into account as exponents of the concentrations.

It is interesting to consider the reactions taking place with an entropy decrease ($\Delta S < 0$): for instance, this is the case of the reactions proceeding with a reduction of the moles number. In such a case, the entropic term ($-T \Delta S$) results in becoming positive, thus reducing the amount of released energy ($-\Delta H$) that can be available for producing work ($-\Delta G$). In other words, when $\Delta S < 0$, a share of the energy released ($-T \Delta S$) is spent to make the system more ordered. Such an amount of energy reduces the spontaneity level expected from the enthalpy change of an exothermic reaction.

The combinations of the changes in enthalpy and entropy in the chemical reactions and the role of the temperature is reported in a simplified way in Figure 2. The possible cases are the following:

- Regardless of the temperature, the reactions with $\Delta H < 0$ and $\Delta S > 0$ are spontaneous, while those with $\Delta H > 0$ and $\Delta S < 0$ are non-spontaneous,
- The reactions with $\Delta H < 0$ and $\Delta S < 0$ are spontaneous for $T < \frac{|\Delta H|}{|\Delta S|}$, while those with $\Delta H > 0$ and $\Delta S > 0$ are spontaneous $T > \frac{|\Delta H|}{|\Delta S|}$.



Figure 2. Changes in enthalpy, entropy, and free Gibbs energy (arbitrary units) in chemical reactions vs. the temperature (arbitrary units): the value of ΔG calculated through the expression (4) is reported along the temperature for the different cases (exothermic/endothermic reactions occurring with positive or negative change in entropy).

In particular, let us consider the exothermic reactions ($\Delta H < 0$), which will be the subject of the following section relating to nuclear processes, where $Q_{value} > 0$ is assumed. At low temperature, these reactions are spontaneous regardless of the change in the entropy, while, with the increasing temperature, the entropy could play a key role in establishing the reaction spontaneity. In fact, the entropic term ($-T \Delta S$) of reactions characterized by a reduction of the moles number ($\Delta S < 0$) increases with the temperature by contributing to the augmentation of the Gibbs free energy change that, finally, could overcome the zero and make the reaction non-spontaneous.

2.2. Classical Thermodynamic Analysis of Nuclear Processes

Once the classic thermodynamic approach used for the evaluation of chemical reactions has been introduced, it is possible to identify what is missing in the feasibility criterion adopted for nuclear reactions, which is based on the evaluation of the Q_{value} . Such a criterion is well-related to the contribution to the reaction spontaneity coming from the change in enthalpy, while it does not provide any information on how the entropic term affects the reaction. When writing the change in Gibbs free energy of a nuclear reaction, something is missing:

$$\Delta G = -Q_{\text{value}} + ? \tag{6}$$

It is noteworthy to discuss the rationale behind such an approach, which could be justified by the analytical differences between fission and fusion reactions once the contribution of the entropic term is evaluated. In principle, moving from the definition of fission and fusion reactions, we expect to have positive change in entropy ($\Delta S > 0$) in fission processes where "heavy nuclei split into smaller fragments": these processes proceed with an increase of the particles number, creating a more disordered system. The opposite situation ($\Delta S < 0$) occurs for fusion processes where "light atoms merge to form a heavier nucleus". Moving from these considerations, the graph of Figure 3 shows the change in Gibbs free energy vs. the temperature for chemical and nuclear reactions.



Figure 3. Change in Gibbs free energy vs. the temperature. Comparison of the behavior of chemical and nuclear reactions. ΔH_{chem} and ΔH_{nucl} indicate the change in enthalpy of chemical and nuclear reactions, respectively. ΔG_{FIS} and ΔG_{FUS} indicate the change in Gibbs free energy of fission and fusion reactions, respectively.

As already introduced, only exothermic nuclear reactions (Q_{value} positive, ΔH negative) are considered in the following. Regardless of the change in entropy, the feasibility criterion based on the assessment of the Q_{value} alone could be justified by the fact that both fission and fusion nuclear reactions are characterized by extremely large energy releases: the enthalpy change of nuclear reaction ($|\Delta H_{nucl}|$) is of the order of 1 MeV per particle, which is much larger than those of chemical reactions ($|\Delta H_{chem}|$), which is around 1 eV per particle. That is, the nuclear reactions exhibit values of change in enthalpy that are very negative (and very large in absolute value)—about six orders of magnitude larger than those of the chemical processes. These large negative values of the change in enthalpy in the nuclear reactions could advise one to pay no attention to the contribution of the change in entropy. Especially, this is reasonable in fission ($\Delta S > 0$) where the entropic term ($-T \Delta S$) is negative: in fact, it can only contribute to further reduce the change in Gibbs free energy and then strengthening the reaction spontaneity.

2.3. The Role of Entropy in Fusion Reactions

In fusion reactions, the entropy change is negative ($\Delta S < 0$) and, therefore, the entropic contribution $(-T \Delta S)$ to the Gibbs free energy change is positive. For instance, in the typical temperature range of chemical and fission processes (100–1000 K), this contribution is much lower than the change in enthalpy ($|T \Delta S| \ll |\Delta H|$): in such a way, the ΔG assumes soundly negative values and the fusion reactions occur spontaneously. Limiting the analysis to low temperature processes, one could believe that the feasibility criterion of having a strongly exothermic nuclear reaction (i.e., the presence of a very large $Q_{value} \approx MeV$) is sufficient to establish its spontaneity from a thermodynamic point of view. However, the realization of fusion power is mostly studied in tokamaks where a plasma of deuterium and tritium, magnetically confined, reacts at very high temperature ($\approx 10^8$ K): under these conditions, the entropic term is very large and could overcome the Q_{value}. As previously discussed, when $\Delta S < 0$, a share of the energy released ($-T \Delta S$) is spent to make the system more ordered then reducing its spontaneity level. The higher the temperature, the more difficult and the more expensive it is to create order (i.e., the larger is the energy that has to be spent to make the system more ordered): this is the case of nuclear fusion, which is carried out in a plasma operated at very high temperatures. In these conditions, the entropic term achieves very high values and, possibly, balances or overcomes the energy released (Q_{value}). In other words, in fusion reactions the temperature acts as a very powerful amplifier of the entropic term $(-T \Delta S)$ that, at a temperature of millions Kelvin, can suck up all the enormous energy released, namely the Q_{value}.

Following the above considerations, the spontaneity of fusion reactions cannot be evaluated through its exothermicity assessment alone but must consider the entropic term in comparison with the Q_{value} . The combination of (5) and (6) leads us to define a limit temperature T* below which the fusion reaction proceeds spontaneously. The temperature T* corresponds to the condition $\Delta G = 0$ and, under the assumptions of processes carried out at constant temperature and pressure, it results in the following:

$$T^* = \frac{Q_{\text{value}}}{|\Delta S|} \tag{7}$$

According to the above discussion, the practicability of fusion reactions from a thermodynamic point of view could be based on the assessment of T*, which acts as a thermodynamic critical temperature.

3. Feasibility Criteria of Fusion Nuclear Reactions

As discussed above, a first criterion for establishing the feasibility of a nuclear reaction relies on the estimation of its Q_{value} , which corresponds to the energy released by the reaction. This factor is commonly adopted in nuclear physics to establish the spontaneity of a process: the larger the positive Q_{value} , the more likely the reaction is shifted towards the products. Particularly, for the fusion reactions, the Q_{value} calculation has to be integrated

with the assessment of the entropic contribution to the Gibbs free energy change. However, such a thermodynamic analysis is effective to describe a system under equilibrium conditions but provides no effective information on the reaction kinetics. For instance, it could happen that a spontaneous reaction ($\Delta G < 0$) exhibits a very low reaction rate and proceeds very slowly, thus making the process unfeasible.

Once the change of the thermodynamic functions has been assessed, it is also necessary to evaluate its reaction rate in order to verify the feasibility of a nuclear process. Both the thermodynamic and kinetic parameters, namely the Gibbs free energy change and the reactivity, will hereafter be evaluated for the most studied deuterium-based fusion reactions. Specifically, the behavior of these parameters vs. the temperature will be discussed by considering the operating conditions of the tokamaks, which are machines designed for the exploitation of fusion power via a deuterium-tritium (DT) plasma magnetically confined at very high temperature.

3.1. Reaction Kinetics

In a nuclear fusion reaction, two positively charged nuclei must come into contact by winning the repulsive Coulomb force. The consequent force field produces a potential barrier of the order of 1 MeV at a distance of approximately the nuclear radius while, below such a distance, the nuclear attractive forces prevail. Although the classical mechanics foresee that only nuclei with energy exceeding the potential barrier can react, the quantum mechanics allows for tunneling through a potential barrier of finite extension. Gamow's theory links the cross section to the tunneling of the Coloumb barrier and then to the probability of the reaction [21]:

$$\sigma\left(\varepsilon\right) = \frac{S\left(\varepsilon\right)}{\varepsilon} e^{\left(-\sqrt{\frac{\varepsilon_{\rm G}}{\varepsilon}}\right)} \tag{8}$$

where $\sigma(\varepsilon)$ is the cross section (arbitrary units) for reacting particles of energy ε (arbitrary units), $S(\varepsilon)$ (arbitrary units) a factor weakly varying in function of the energy, and ε_G which is the Gamow energy that in practice acts as an energy barrier.

The reactivity, which is related to the likelihood that a reaction occurs, assesses the probability of reaction per unit time and unit density of the target nuclei. It is evaluated by the product of the cross section (σ) and the particle velocity (v). Usually, for the fusion reactions an averaged reactivity $\langle \sigma v \rangle$ is calculated by taking into account the velocity distribution of the particles according to experimental data [25] or by using specific models, as in the case of the Maxwell-averaged reactivity [26,27].

3.2. Entropy Assessment

The assessment of the thermodynamic functions (G, H, S) for the chemical processes relies on the availability of a complete database reporting these values for the chemical elements. Following the thermodynamic rules, it is in turn easy to calculate the values of the thermodynamic functions for all the possible molecules and compounds involved in the studied processes [24]. However, several particles involved in nuclear reactions consist of isotopes and nucleons (neutrons, protons) that are not considered in the available thermodynamic database: in this case, it is needed to establish an alternative approach to assess their thermodynamic functions change.

As seen, most of the energy released from a nuclear reaction is at the end turned into heat and its enthalpy change could be estimated to a good approximation by the Q_{value} , as defined by Formula (2).

The assessment of the entropy can be done via statistical thermodynamic methods: such an approach has been used to calculate the entropy of "compound nucleuses", which are intermediate compounds consisting of target nucleuses and the projectiles of nuclear reactions in excited states [28,29]. The evaluation of the statistical analogous of thermodynamic properties moves from the assessment of the partition function of the system (Q) at constant temperature and volume. In turn, the entropy (S) is related to Q by the following expression [24]:

$$S = k \cdot \left[\frac{\partial T \ln(Q)}{\partial T} \right]_{N,V}$$
(9)

where k is the Boltzmann constant and T the absolute temperature. For a perfect gas, the partition function is given by:

 $Q = \frac{1}{N!} \cdot V^{N} \left(\frac{2 \cdot \pi \cdot \mathbf{m} \cdot \mathbf{k} \cdot \mathbf{T}}{h^{2}} \right)^{\frac{3}{2}N} (\mathbf{f}^{\text{int}})^{N}$ (10)

where N is the number of particles, m their mass, h the Plank constant, and f^{int} is the partition function of each particle (or molecule). For monoatomic compounds, f^{int} is equal to 1.

Combining the above expressions, the Sackur–Tetrode equation is obtained:

$$S = n \cdot R \cdot \left[ln \left(\frac{M^{\frac{3}{2}} \cdot T^{\frac{5}{2}}}{P} \right) - 1.16 \right]$$
(11)

where n is the number of moles (1 mole = 6.022×10^{23} particles), P is the pressure (atm), M the molecular weight, and R the gas constant.

4. Results

The realization of the fusion energy via magnetic-confinement devices is focused on the exploitation of deuterium-based reactions. The most studied reaction is that between deuterium (D) and tritium (T), which react to form ⁴He and a neutron:

$$^{2}_{1}H + ^{3}_{1}H = ^{4}_{2}He + ^{1}_{0}n \qquad Q_{value} = 17.586 \text{ MeV}$$
 (12)

The other fusion reaction studied is that between two deuterium atoms. It has two branches, both with branching ratio around 0.50. The first one produces tritium and a proton:

$$^{2}_{1}H + ^{2}_{1}H = ^{3}_{1}H + ^{1}_{1}p \qquad Q_{value} = 4.032 \text{ MeV}$$
 (13)

and the second one produces ³He and a neutron:

$$^{2}_{1}H + ^{2}_{1}H = ^{3}_{2}He + ^{1}_{0}n \qquad Q_{value} = 3.2674 \text{ MeV}$$
(14)

Finally, a fourth reaction between deuterium and ³Helium is considered in this study:

$$^{2}_{1}H + ^{3}_{2}He = ^{4}_{2}He + ^{1}_{1}p \qquad Q_{value} = 18.351 \text{ MeV}$$
 (15)

4.1. Reactivity of the D-Based Reactions

The reactivity of these D-based reactions is shown in the graph of Figure 4, in which the temperature is measured in keV (1 keV/ $k_B = 1.16 \times 10^7$ K, where k_B is the Boltzmann constant). In fact, in nuclear physics the temperature of particles is usually expressed in terms of the energy that corresponds to the center-of-mass of their velocity distribution.

Among the D-based reactions, the reaction (1) exhibits the highest reactivity and it is the main process considered in the designs of future fusion power plants. In these reactors, the tritium is produced by a Li-based breeding blanket surrounding the plasma chamber where the deuterium–tritium is heated at around 1.5×10^8 K ≈ 13 keV [30,31]. At this temperature, the reactivity of the reaction (1) is around 1.91×10^{-22} m³/s, which is higher than that of the reactions (2) and (3) (both around 1×10^{-24} m³/s) and of the reaction (4) (around 7.40×10^{-25} m³/s).



Figure 4. Values of the Maxwell-averaged reactivities " σ v" of D-based reactions calculated from literature [26,27]. "DT" is indicating the reaction (12), "DD -> p" the reaction (13), "DD -> n" the reaction (14) and "D³He" the reaction (15).

4.2. Entropy of the D-Based Reactions

The Sackur–Tetrode equation can be used to assess the entropy of fusion reactions of interest for applications in the tokamaks under the hypothesis that the reacting particles, at plasma state, behave as a perfect gas.

Moreover, the Equation (11) is not appropriate to the sub-nuclear particles as those involved in the fusion reactions (neutrons, protons, etc.). The Sackur–Tetrode equation can be applied only to atoms and, therefore, the initial and final states of the fusion reactions have to be selected in order to comply with this condition.

For the four D-based reactions considered, the initial state consists of two monoatomic atoms (deuterium, ⁴He, tritium, ³He) at high temperature and pressure of 5×10^{-5} atm (\approx 5 Pa), a value in agreement with both experiments and designs of magnetic fusion devices [32,33]. Under these conditions, the Sackur–Tetrode equation can be effectively applied.

In order to comply with the Sackur–Tetrode equation, the final state of the reactions (12)–(15) has been chosen under the assumption that their products (atoms of helium and tritium, protons, and neutrons) have interacted with the system's walls and changed their energy into heat. Such a condition could be verified in a tokamak surrounded by shielding walls where the energy released by the nuclear reactions is extracted through a cooling system at 700 K, a temperature representative of shielding and blanket systems of the magnetically confined fusion devices [34]. With the aim to highlight the final state considered, the reactions (12)–(15) can be rewritten as follows:

$$D + T = {}^{4}He + 17.586 \text{ MeV}$$
(16)

$$D + D = T + 4.032 \text{ MeV}$$
 (17)

$$D + D = {}^{3}He + 3.2674 \text{ MeV}$$
(18)

$$D + {}^{3}He = {}^{4}He + 18.351 \text{ MeV}$$
(19)

As in the Sackur–Tetrode expression, the change of pressure has a modest influence on the entropy assessment, and its variation was not taken into consideration.

The change in Gibbs free energy between the initial and final states above-defined can be evaluated by the following expression:

$$\Delta G = \Delta H - \Delta (TS) \tag{20}$$

In this calculation, the initial and the final state correspond to the reactants at the generic temperature T and the products at 700 K, respectively. The change in enthalpy is given by the Q_{value} and the expression (20) becomes:

$$\Delta G = -Q_{\text{value}} - [(700 \, \text{S}_{700 \, \text{K}} - \text{T} \, \text{S}_{\text{T}})] \tag{21}$$

where S_{700K} and S_T are the values of the entropy calculated via the Sackur–Tetrode equation at 700 K and at the reactants' temperature T (K), respectively.

The thermodynamic critical temperature T*, previously introduced and defined by the equilibrium condition $\Delta G = 0$, is obtained by solving the expression:

$$Q_{\text{value}} = [T S]_{700 \text{ K}} - [T S]_{T^*}$$
(22)

In the following sections, to directly compare the effect of the temperature on the thermodynamics and kinetics of the reactions studied, the Δ G values calculated by the expression (21) are reported together with those of the reactivity (Figures 5–8).



Figure 5. Reactivity (square and black line) and change of Gibbs free energy (blue line) vs. temperature for the deuterium–tritium reaction (the red dashed line indicates $\Delta G = 0$: below it the reaction occurs spontaneously).



Figure 6. Reactivity (square and black line) and change in Gibbs free energy (blue line) vs. temperature for the deuterium–deuterium reaction branch to produce Tritium and a proton (the red dashed line indicates $\Delta G = 0$: below it the reaction occurs spontaneously).



Figure 7. Reactivity (square and black line) and change in Gibbs free energy (blue line) vs. temperature for the deuterium–deuterium reaction branch to produce ³Helium and a neutron (the red dashed line indicates $\Delta G = 0$: below it the reaction occurs spontaneously).



Figure 8. Reactivity (square and black line) and change in Gibbs free energy (blue line) vs. temperature for the deuterium–³helium reaction (the red dashed line indicates $\Delta G = 0$: below it the reaction occurs spontaneously).

4.3. Deuterium-Tritium Reaction

The deuterium–tritium (DT) reaction is the most studied fusion reaction in the magnetically confined machines, in which the plasma is operated at around 13 keV (1.5×10^8 K) [19]. As shown in Figure 5, this reaction exhibits the maximum reactivity (about 9.1×10^{-22} m³/s) at 64 keV (7.42×10^8 K) while the limit temperature T* is 1.32×10^2 keV (1.58×10^9 K). The operation at this temperature is very challenging from an engineering point of view and will need the development of special technologies and materials. At this temperature, the reactivity is about 2×10^{-22} m³/s, which is around one fourth of the maximum one: such a value is considered enough to realize a tritium burn fraction (i.e., the amount of tritium burned in the plasma before confinement is lost) that is capable guaranteeing the tritium self-sufficiency conditions of the fusion reactors [35-37]. At 13 keV (1.5×10^8 K) the change in Gibbs free energy is -16.0 MeV, demonstrating the sound spontaneity of this reaction. Around the maximum of its reactivity (64 keV or 7.42×10^8 K), the Δ G of the DT reaction is -9.51 MeV, thus exhibiting a good spontaneity.

4.4. Deuterium–Deuterium Reaction to Produce Tritium and a Proton

The first branch of the reaction deuterium–deuterium (DD) produces tritium and a proton: it exhibits a poor spontaneity ($\Delta G = -2.53$ MeV) at the tokamaks' temperature (13 keV or 1.5×10^8 K) that is very close to its limit temperature T* (33.4 keV or 3.88×10^8 K); see Figure 6. The maximum reactivity of 1.76×10^{-22} m³/s is achieved at much higher temperatures (1250 keV or 1.45×10^{10} K): in these conditions, the ΔG becomes positive (+1.70 $\times 10^2$ MeV) and the reaction is not spontaneous. In practice, the thermodynamic spontaneity of this reaction is correlated to very low kinetics, and vice versa.

4.5. Deuterium–Deuterium Reaction to Produce ³Helium and a Neutron

The second branch of the reaction DD produces ³Helium and a neutron and is characterized by values of ΔG and a reactivity very similarly to those of the first DD branch; see Figure 7. The application of the Sackur–Tetrode equation to the reactions (13) and (14) leads to the calculation of the same values of change in entropy and, therefore, the change in Gibbs free energy for these two reactions is very similar. It differs by about 0.76 MeV, due to the slightly different contribution to the ΔG coming from the Q_{value}, which is 4.032 MeV and 3.267 MeV for the reactions (13) and (14), respectively.

The limit temperature T* is 26.7 keV (3.10×10^8 K) while at the tokamaks' temperature the ΔG is -1.77 MeV. The reactivity maximum of 2.19×10^{-22} m³/s is achieved at higher temperatures (1750 keV or 2.03×10^{10} K): in these conditions, the ΔG is positive (+2.43 $\times 10^2$ MeV) and the reaction turns out to be non-spontaneous.

4.6. Deuterium–³Helium Reaction

As reported in Figure 8, the reaction D^3 He is characterized by values of change in Gibbs free energy that are very similar to those of the reaction DT. In fact, the Sackur–Tetrode equation assesses the same values of entropy for the reactions (16) and (19): their ΔG differ by 0.76 MeV, i.e., the difference of their Q_{value}, 17.586 MeV and 18.351 MeV, respectively for the DT and the D³He reactions. As discussed previously, the reactivity of the reaction D³He is lower than that of reaction DT, which is at least two orders of magnitude at the tokamaks' temperature, i.e., about 10^{-24} m³/s (for DT) against 10^{-22} m³/s (for D³He).

The limit temperature T* is one order of magnitude higher $(1.42 \times 10^2 \text{ keV or } 1.65 \times 10^9 \text{ K})$ than the tokamak's temperature, at which the reaction exhibits a large spontaneity $(\Delta G = -16.8 \text{ MeV})$. The reactivity maximum of $3.96 \times 10^{-22} \text{ m}^3/\text{s}$ is achieved at 250 keV $(2.90 \times 10^9 \text{ K})$: in these conditions, the ΔG is positive (+9.81 MeV) and the reaction is not spontaneous. As for the two DD reactions, it is not possible to simultaneously maximize the thermodynamic spontaneity and the reaction kinetics. From Figure 8, it is possible to see the effect of the temperature on the ΔG and the reactivity: when increasing the temperature by one order of magnitude from 10^1 to 10^2 keV the reactivity moves from 10^{-25} to $10^{-22} \text{ m}^3/\text{s}$ while the ΔG passes from -17.2 to -5.67 MeV. This means that when increasing the temperature from 10^1 to 10^2 keV, the entropic term ($-T \Delta S$) absorbs 11.5 MeV of the Q_{value} and, therefore, a large fraction of the energy released by the reaction is spent to make the system more ordered.

5. Discussion

The four D-based reactions (16)–(19) are characterized by a limit temperature T* higher than 1.5×10^8 K (≈ 13 keV), the operating temperature foreseen in the tokamaks, which are devices in which a plasma of hydrogen isotopes is magnetically confined to exploit fusion energy. From a thermodynamic point of view, all the fusion reactions considered here are feasible, although with different levels of spontaneity.

At the tokamak's temperature 1.5×10^8 K (≈ 13 keV), the two branches of the DD reaction exhibit poor performance in terms of both thermodynamic spontaneity and reactivity. Borrowing the jargon used by chemists, we could say that in tokamak devices the DD plasma reacts a little (i.e., only few D atoms react to produce ³He or tritium) and very slowly, at least two orders of magnitude less than the DT reaction does. Furthermore, any change of the temperature is ineffective to improve the reaction feasibility: the temperature should increase to improve the reaction kinetics but in this way the reaction conversion should further reduce by making the process non-spontaneous, and vice versa. In fact, the higher the temperature, the higher the probability that the atoms react according to the expression (8) but, simultaneously, the higher the share of the energy released by the reaction (Q_{value}) that has to be spent to make the system more ordered (" $-T \Delta S$ ").

The reaction DT is the most promising among those considered for exploiting the fusion energy in tokamaks: it exhibits a sound spontaneity with a value $\Delta G = -16.0 \text{ MeV}$ at $1.5 \times 10^8 \text{ K}$ ($\approx 13 \text{ keV}$), a temperature that is close to its reactivity maximum (about $9.1 \times 10^{-22} \text{ m}^3/\text{s}$) occurring at 64 keV ($7.42 \times 10^8 \text{ K}$). Such values of reactivity correspond to a modest probability of reaction that, however, is considered enough to guarantee both the tritium self-sufficiency and the tritium burning rate needed to operate the fusion power plants with a net energy production.

In principle, there are several aspects that make D³He with respect to DT an appealing choice: the use of a non-radioactive fuel (³He instead of tritium) and the possibility to directly convert a part of the plasma energy into electricity [38–40]. Further, for the D³He reaction the development of the reactor materials is less challenging than for the DT one due to the smaller neutron damages and the absence of the breeding blanket. The D³He reaction exhibits ΔG values very close to those of the DT reaction: in fact, their limit temperatures T* are 1.42×10^2 keV (1.65×10^9 K) and 1.32×10^2 keV (1.58×10^9 K), respectively, which are both well-above the tokamaks' temperature.

On the contrary, the D^3 He reaction kinetics is near that of the DD reactions: at the tokamaks' temperature, its reactivity is of the order of 10×10^{-24} m³/s, which is at least two orders of magnitude lower than that of the DT reaction. Differently from the DD reactions, in this case there is a margin to take advantage of regarding the temperature increase in order to improve the reaction kinetics. In fact, close to its limit temperature $(1.42 \times 10^2 \text{ keV or } 1.65 \times 10^9 \text{ K})$ the reactivity rises to about 10^{-22} m³/s, which are values corresponding to the reactivity of the DT reaction studied in the tokamak devices. However, in these conditions the energy made available reduces significantly, from -16.8 MeV (at the tokamak temperature) to few MeV, making the reaction less competitive from an energy point of view. Furthermore, for achieving the DT reaction performances, the D³He reaction should address several complications, mainly due to the much higher plasma confinement and plasma pressure, which have never been demonstrated experimentally.

In the limits of the assumptions done, this study demonstrates that the D-based reactions considered and, particularly, the DT reaction, are thermodynamically spontaneous at the tokamaks' temperature. However, as a final remark, this analysis provides evidence that, from a thermodynamic point view, the operation at a very high temperature (such as for the hot plasmas) acts to reduce the feasibility of the fusion processes. In fact, the higher the temperature, the higher the share of the energy released by the fusion reaction that is absorbed by the entropic term. These considerations suggest maintaining the development of alternative systems where the energy needed to win the kinetic barriers is provided to the reactants at temperatures as low as possible.

6. Summary, Conclusions, and Outlook

This thermodynamic analysis of nuclear reactions demonstrates the different roles played by entropy in fission and fusion processes. In particular, in the fusion reactions the operation at a very high temperature could involve a positive change in Gibbs free energy and then making the process non-spontaneous. In the fusion reactions that are studied in tokamak devices where a magnetically confined plasma is heated at millions Kelvin, the temperature acts as a very powerful amplifier of the entropic term ($-T \Delta S$), which could absorb all the energy corresponding to the Q_{value} . The concept of a limit temperature T* has been introduced as a thermodynamic criterion for establishing the feasibility of these nuclear processes. It is the temperature at which the ΔG equals to zero, i.e., indicating the passage from a spontaneous process ($\Delta G < 0$) to a non-spontaneous one ($\Delta G > 0$).

The assessments carried out in this work have considered four deuterium-based fusion reactions of potential interest for exploiting the fusion energy on the Earth.

At the tokamaks' temperature, the two branches of the DD reaction exhibit a modest spontaneity (ΔG around -2 MeV) coupled to very low reactivity values (10^{-24} m³/s). However, raising the temperature to increase the reactivity would be ineffective in improving the feasibility of the reaction as it would also increase the entropic term, thus shifting the ΔG towards positive values. The D³He reaction at the tokamaks' temperature exhibits reactivity values similar to those of the DD one (around 10^{-24} m³/s), but has a limit temperature of 1.65×10^9 K, which is about two orders of magnitude higher than that of tokamaks. In this case, an increase of the plasma temperature could augment the reactivity up to values of 10^{-22} m³/s, which are considered enough for the operations of the tokamaks designed for the DT reaction. However, these operating conditions significantly

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reduce the energy made available by the D³He reaction and would require the achievement of a plasma confinement and control that have never been demonstrated experimentally.

Finally, this analysis confirms that the DT reaction is the most promising fusion reaction to be realized through tokamak devices. At the temperature of 1.5×10^8 K (≈ 13 keV) the DT reaction shows a large thermodynamic spontaneity coupled with reactivity values of the order of 10^{-22} m³/s.

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References

- 1. 2021 Strategic Foresight Report—The EU's Capacity and Freedom to Act. Available online: https://ec.europa.eu/info/sites/defa ult/files/strategic_foresight_report_2021_en.pdf (accessed on 5 May 2023).
- bp Statistical Review of World Energy 2022—71st Edition. Available online: https://www.google.com/url?sa=t&rct=j&q=&esrc= s&source=web&cd=&ved=2ahUKEwjen5uc44z8AhV0RvEDHQhzA2oQFnoECBcQAQ&url=https%3A%2F%2Fwww.bp.com% 2Fcontent%2Fdam%2Fbp%2Fbusiness-sites%2Fen%2Fglobal%2Fcorporate%2Fpdfs%2Fenergy-economics%2Fstatistical-revi ew%2Fbp-stats-review-2022-full-report.pdf&usg=AOvVaw1M37w1Au6qujo7XTIb-KW8 (accessed on 5 May 2023).
- Sustainable Development Goals (SDGs). Available online: https://unric.org/en/united-nations-sustainable-development-goals/ (accessed on 5 May 2023).
- 4. Marseglia, G.; Rivieccio, E.; Medaglia, C.M. The dynamic role of Italian Energy strategies in the worldwide scenario. *Kybernetes* **2019**, *48*, 636–649. [CrossRef]
- Capurso, T.; Stefanizzi, M.; Torresi, M.; Camporeale, S.M. Perspective of the role of hydrogen in the 21st century energy transition. Energy Convers. Manag. 2022, 251, 114898. [CrossRef]
- 6. Maestre, V.M.; Ortiz, A.; Ortiz, I. Challenges and prospects of renewable hydrogen-based strategies for full decarbonization of stationary power applications. *Renew. Sustain. Energy Rev.* **2021**, 152, 111628. [CrossRef]
- 7. Trelles, J.P. Solar-plasma reactors for CO₂ conversion. J. Phys. D Appl. Phys. 2022, 55, 103001. [CrossRef]
- Tosti, S.; Pozio, A.; Farina, L.; Santucci, A. Hydrogen and Oxygen Production via Water Splitting in a Solar-Powered Membrane Reactor—A Conceptual Study. *Hydrogen* 2021, 2, 18–32. [CrossRef]
- Nuclear Power in a Clean Energy System, IEA Report, May 2019. Available online: https://iea.blob.core.windows.net/assets/a d5a93ce-3a7f-461d-a441-8a05b7601887/Nuclear_Power_in_a_Clean_Energy_System.pdf (accessed on 5 May 2023).
- 10. Li, C.-j.; Zhang, C.-m.; Chen, Y.; Zuo, J.-x.; Chen, J.-y. The Study on Safety Goals and Public Acceptance of Nuclear Power. *Energy Procedia* **2013**, *39*, 415–422.
- 11. Roh, S.; Kim, D. The relationship between public acceptance of nuclear power generation and spent nuclear fuel reuse: Implications for promotion of spent nuclear fuel reuse and public engagement. *Nucl. Eng. Technol.* **2022**, *54*, 2062–2066.
- 12. Artsimovich, L. The Road to Controlled Nuclear Fusion. Nature 1972, 239, 18–22. [CrossRef]
- 13. Toschi, R. Nuclear fusion, an energy source. Fusion Eng. Des. 1997, 36, 1–8. [CrossRef]
- 14. Ongena, J. Fusion: A true challenge for an enormous reward. *EPJ Web Conf.* 2018, 189, 00015. [CrossRef]
- 15. Moir, R.W. Feasibility study of a magnetic fusion production reactor. J. Fusion Energy 1986, 5, 257–269. [CrossRef]
- 16. Carruthers, R. The Fusion Dilemma. Interdiscip. Sci. Rev. 1981, 6, 127–141. [CrossRef]
- 17. Sheffield, J. Physics requirements for an attractive magnetic fusion reactor. Nucl. Fusion 1985, 25, 1733. [CrossRef]
- 18. Parkins, W.E. Energy. Fusion Power: Will It Ever Come? Science 2006, 311, 16527955. [CrossRef]
- 19. Ongena, J.; Koch, R.; Wolf, R.; Zohm, H. Magnetic-confinement fusion. Nat. Phys. 2016, 12, 398–410. [CrossRef]
- Campbell, D.J.; Akiyama, T.; Barnsley, R.; Bassan, M.; Baylor, L.R.; Bertalot, L. Innovations in Technology and Science R&D for ITER. J. Fusion Energy 2019, 38, 11–71. [CrossRef]
- 21. Atzeni, S.; Meyer-ter-Vehn, J. *The Physics of Inertial Fusion: Beam Plasma Interaction, Hydrodynamics, Hot Dense Matter;* Oxford University Press: Oxford, UK, 2008. [CrossRef]
- 22. Tosti, S. Spontaneity of Nuclear Fusion: A Qualitative Analysis via Classical Thermodynamics. *Open Res. Eur.* **2021**, *1*, 67. Available online: https://open-research-europe.ec.europa.eu/articles/1-67 (accessed on 5 May 2023). [CrossRef]
- Tosti, S.; Marrelli, L. Classical Thermodynamic Analysis of Deuterium-Based Fusion Reactions. *Hydrogen* 2022, *3*, 53–61. Available online: https://www.mdpi.com/2673-4141/3/1/4 (accessed on 5 May 2023). [CrossRef]
- 24. Denbigh, K.G. *The Principles of Chemical Equilibrium: With Applications in Chemistry and Chemical Engineering*; Cambridge University Press: Cambridge, UK, 1981. [CrossRef]
- 25. Bosch, H.-S.; Hale, G.M. Improved Formulas for Fusion Cross-Sections and Thermal Reactivities. *Nucl. Fusion* **1992**, *2*, 611. Available online: https://iopscience.iop.org/article/10.1088/0029-5515/32/4/I07/pdf (accessed on 5 May 2023). [CrossRef]

- Hively, L.M. Convenient Computational Forms for Maxwellian Reactivities. *Nucl. Fusion* 1977, 17, 873. Available online: https://iopscience.iop.org/article/10.1088/0029-5515/17/4/019 (accessed on 5 May 2023). [CrossRef]
- 27. Hively, L.M. A simple computational form for Maxwellian reactivities. Nucl. Technol. Fusion 1983, 3, 199–200. [CrossRef]
- 28. Isvoranu, D.; Badescu, V. Radiation exergy: The case of thermal and nuclear energy. *Int. J. Nucl. Gov. Ance Econ. Ecol.* 2008, 2, 90–112. [CrossRef]
- 29. Badescu, V. Exergy of nuclear radiation—A quantum statistical thermodynamics approach. *Open Phys.* **2009**, *7*, 141–146. [CrossRef]
- 30. Siccinio, M.; Biel, W.; Cavedon, M.; Fable, E.; Federici, G.; Janky, F.; Lux, H.; Maviglia, F.; Morris, J.; Palermo, F.; et al. DEMO physics challenges beyond ITER. *Fusion Eng. Des.* **2020**, *156*, 111603. [CrossRef]
- 31. Kembleton, R. Technological features of a commercial fusion power plant, and the gap from DEMO. *Fusion Eng. Des.* **2023**, 190, 113544. [CrossRef]
- Garcia, J.; Challis, C.; Gallart, D.; Garzotti, L.; Görler, T.; King, D.; Mantsinen, M.; JET Contributors. Challenges in the Extrapolation from DD to DT Plasmas: Experimental Analysis and Theory Based Predictions for JET-DT. *Plasma Phys. Control. Fusion* 2017, 59, 014023. Available online: https://iopscience.iop.org/article/10.1088/0741-3335/59/1/014023 (accessed on 5 May 2023). [CrossRef]
- Giegerich, T.; Day, C.; Gliss, C.; Luo, X.; Strobel, H.; Wilde, A.; Jimenez, S. Preliminary configuration of the torus vacuum pumping system installed in the DEMO lower port. *Fusion Eng. Des.* 2019, 146, 2180–2183. [CrossRef]
- Cismondi, F.; Boccaccini, L.V.; Aiello, G.; Aubert, J.; Bachmann, C.; Barrett, T.; Zanino, R. Progress in EU Breeding Blanket design and integration. *Fusion Eng. Des.* 2018, 136, 782–792. [CrossRef]
- 35. Abdou, M.; Riva, M.; Ying, A.; Day, C.; Loarte, A.; Baylor, L.R. Physics and technology considerations for the deuterium–tritium fuel cycle and conditions for tritium fuel self sufficiency. *Nucl. Fusion* **2021**, *61*, 013001. [CrossRef]
- Xie, H.; Chan, V.S.; Ding, R.; Shi, N.; Jian, X.; Zagórski, R.; Li, J.; The CFETR Team. Evaluation of tritium burnup fraction for CFETR scenarios with core-edge coupling simulations. *Nucl. Fusion* 2020, 60, 046022. [CrossRef]
- 37. Day, C.; Battes, K.; Butler, B.; Davies, S.; Farina, L.; Frattolillo, A.; George, R.; Giegerich, T.; Hanke, S.; Hartl, T.; et al. The pre-con cept design of the DEMO tritium, matter injection and vacuum systems. *Fusion Eng. Des.* **2022**, *179*, 113139. [CrossRef]
- 38. Mazzucato, E. A First Generation Fusion Reactor Using the D-3He Cycle. Fusion Sci. Technol. 2021, 77, 173–179. [CrossRef]
- 39. Stott, P.E. The feasibility of using D–3He and D–D fusion fuels. Plasma Phys. Control Fusion 2005, 47, 1305–1338. [CrossRef]
- 40. De Temmerman, G. The helium bubble: Prospects for 3He-fuelled nuclear fusion. *Future Energy Joule* 2021, *5*, 1312–1315. [CrossRef]

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